

Resolved-Rate Motion Control.

Assume a low-level joint controller exists.

It can accurately execute trajectories designed by methods of Chapter 3.

Suppose recent sensor input suggests that the robot end-effector should move in a particular direction at a given speed.

How would one implement this high-level controller.

$$v = J(q) \dot{q}$$

v^* - desired end-effector twist

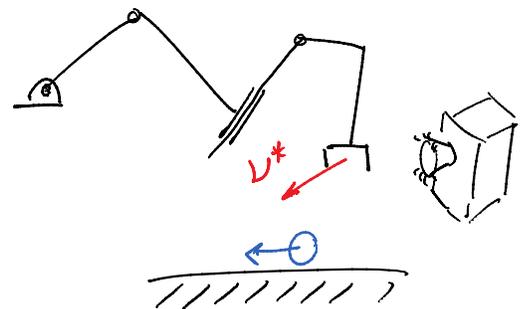
What is desired joint displacement rate, \dot{q}^* ?

$$\dot{q}^* = J^{-1} v^*$$

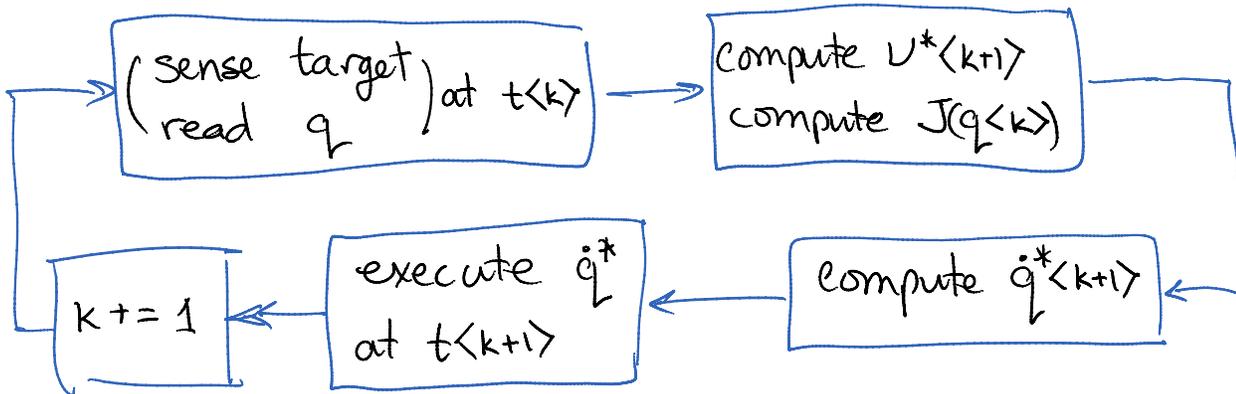
Controller is runs on real-time OS.

Let k be the time step.

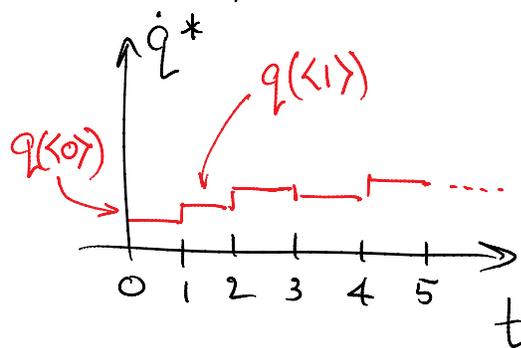
Grab rolling ball



Consider 1 time step in a visual servoing task:



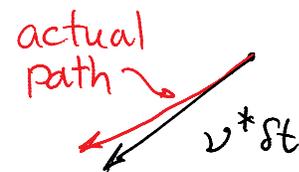
Note: \dot{q}^*_{k+1} is executed until t_{k+2}



If API gives access to positions of joints but not velocities, then use known controller period δt to convert \dot{q}^* to $\delta q^* = \dot{q}^* \delta t$.

$$q_{k+1} = J^{-1}(q_{k+1}) v^* \delta t + q_{k+1}$$

Note: For both approaches, J 's dependence on $q \Rightarrow$ trajectories will drift.



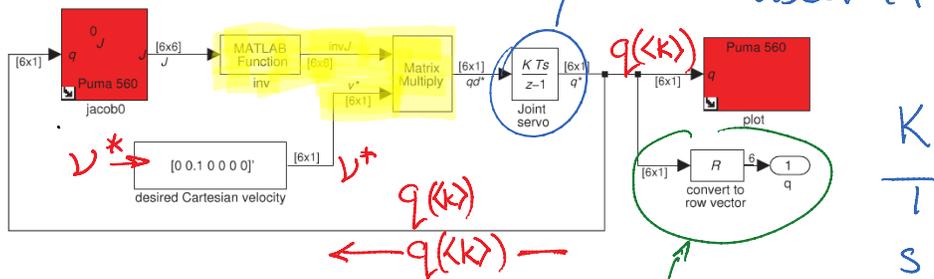
Note: Drift will be worst near singular configurations.

Simulink block diagram

>> sl_rrmc

>> r = sim('sl_rrmc')

z is a discrete-time variable used in control analysis.



Data output

$J \setminus v^*$ is faster than $J^{-1} v^*$

If one used above approach to execute long preplanned trajectories, drift can be significant.

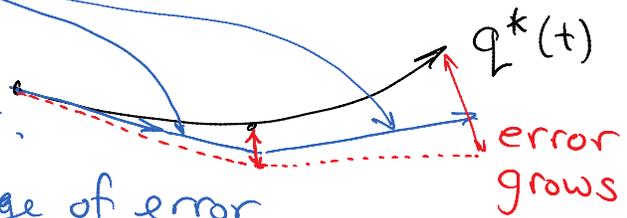
How do we eliminate drift?

Compute error and insert correction.

Consider two steps along $q^*(t)$, an underlying desired trajectory in SE(3).

First method: $\delta q^* = \bar{J}^{-1}(q^{(k)}) v^*$

1. compute tangent.
2. try to move along it.
3. repeat (w/o knowledge of error)



Second method (w/error correction)

$$q^{(k+1)*} = \bar{J}^{-1}(q^{(k)*}) \cdot \delta q$$

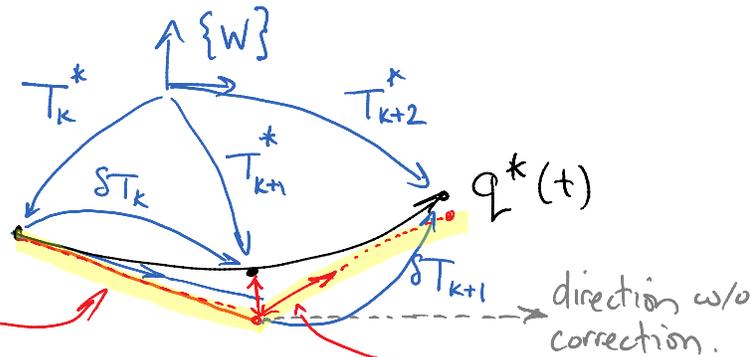
but δq is computed differently:

$$T_k^* \delta T_k = T_{k+1}^*$$

$$\delta T_k = (T_k^*)^{-1} T_{k+1}^*$$

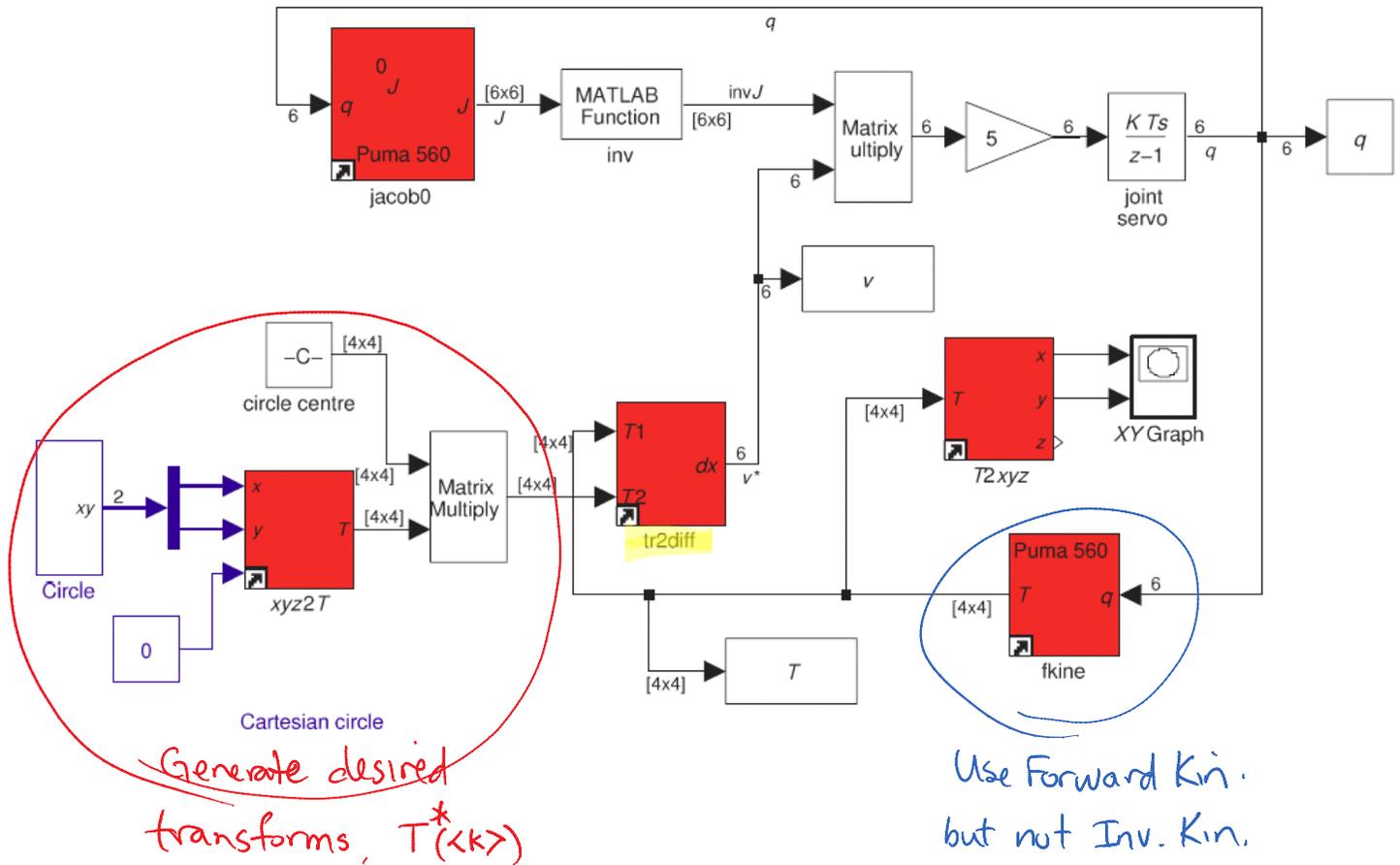
$v^* \delta t$ is replaced by

$$\text{tr2diff}(\delta T) \delta t$$



Step with no initial error is the same

Step with initial error has component to remove error.

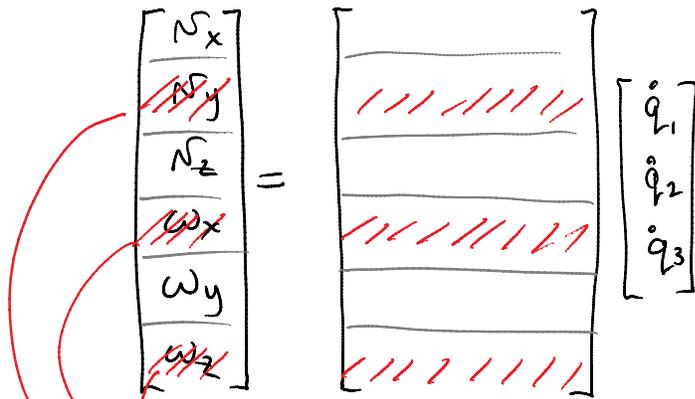


Note: When J^{-1} method must be modified.

The simplest idea

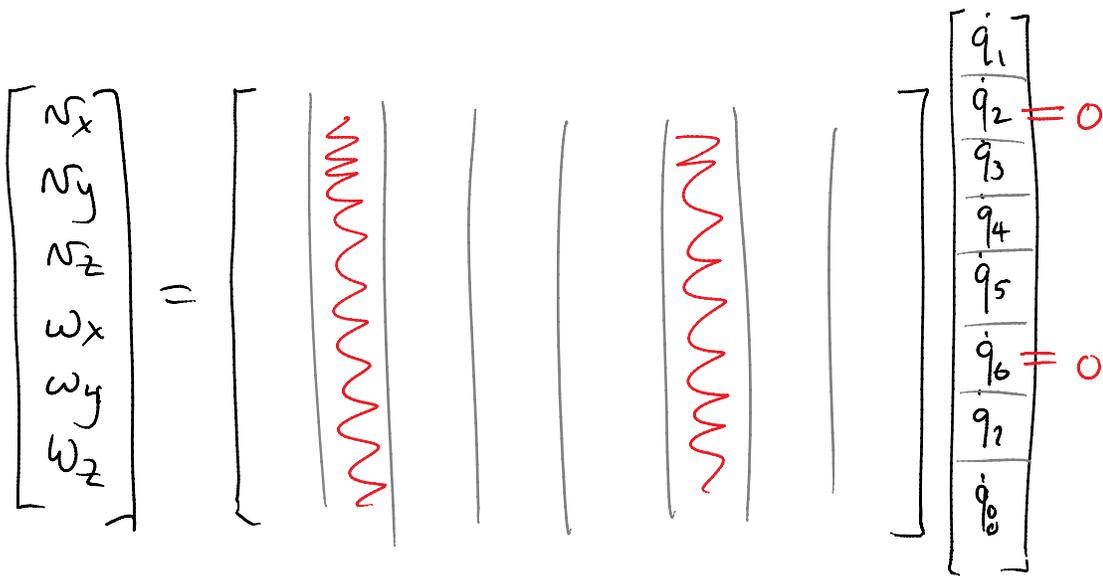
Underactuated: $\dot{v} = J \dot{q}$ delete some rows of J !

Redundant: (over-actuated) $\dot{v} = J \dot{q}$ delete some columns of J !



What should be eliminated?

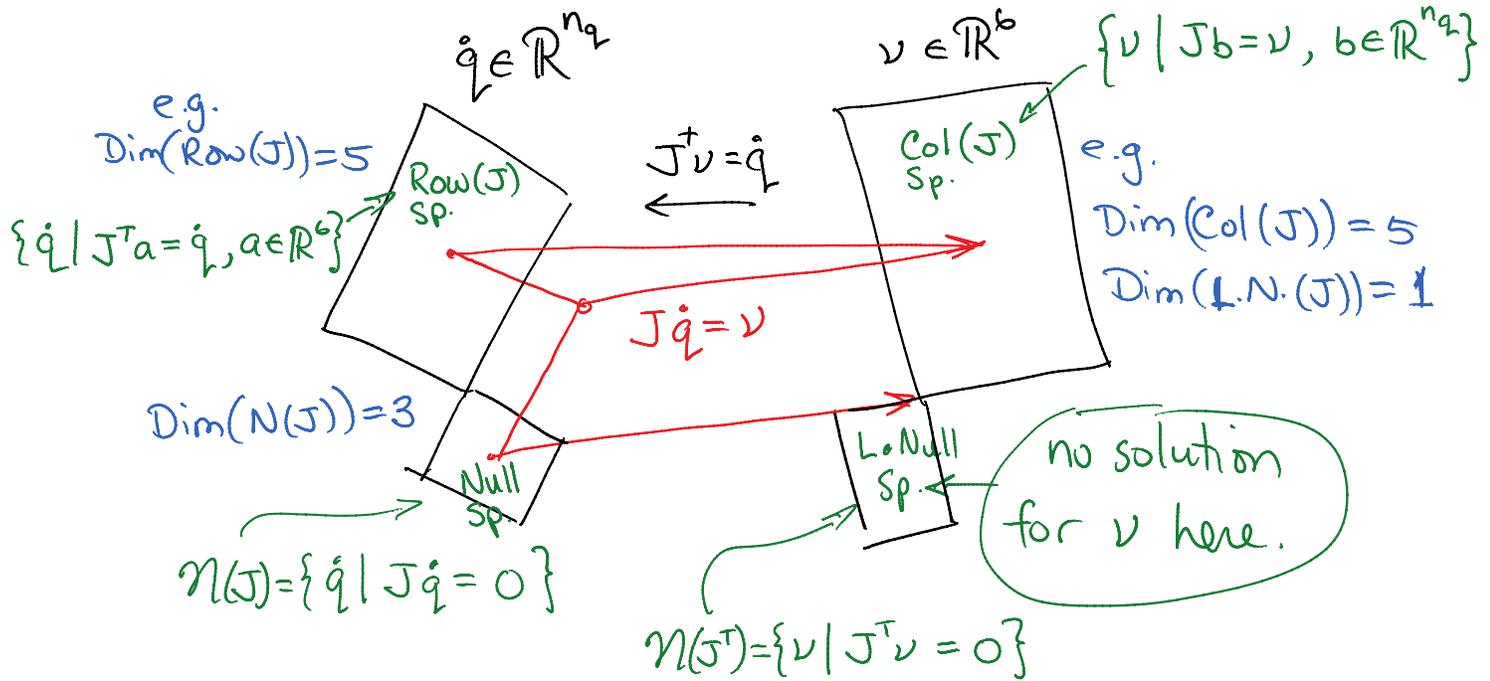
Maybe these are least important.
Resulting J is (3x3).



Perhaps lock some joints!
Resulting J is (6x6).

Pseudo-inverse.

When J is singular, $\nexists J^{-1}$, and \dot{q} may $\nexists \ni J\dot{q} = v^*$.



Case 1: $\text{Rank}(J) < 6 \Rightarrow \text{Dim}(\text{L.N.}(J)) > 0$
 No solution for $v \in \text{L.N.}(J)$

$$\text{Rank}(J) \leq \min(\text{nrows}, \text{ncols})$$

Two main options:

A) Eliminate rows of J until submatrix is non-singular

B.) Use $\dot{q}^* = J^+ v^*$

$\hookrightarrow \text{pinv}(J) \leftarrow \text{pseudo-inverse}$

$$\dot{q}^* \text{ minimizes } \|J\dot{q}^* - v^*\|$$

Case 2: $\text{Rank}(J) = 6 \Rightarrow \text{Dim}(\text{Null}(J)) > 0$

$$\text{Dim}(\text{L.N}(J)) = 0$$

Solution exists $\forall v \in \mathbb{R}^6$

$$\dot{q}^* = J^+ v^* + \underbrace{\mathcal{N}(J)}_{\substack{\text{Null space basis} \\ \text{vectors.}}} \underbrace{\dot{q}_{ns}}_{\text{arbitrary values}}$$

$\text{Dim}(\text{Null}(J)) = \eta = \text{"nullity" of } J.$

$$\dot{q}_{ns} \in \mathbb{R}^\eta.$$

You can choose \dot{q}_{ns} to optimize a desirable motion metric.

$$\text{e.g. } \min \|\dot{q}^*\| \Rightarrow \dot{q}_{ns} = 0$$